

SCALE UP OF STRUCTURED CATALYSTS FOR AMMONIA SYNTHESIS

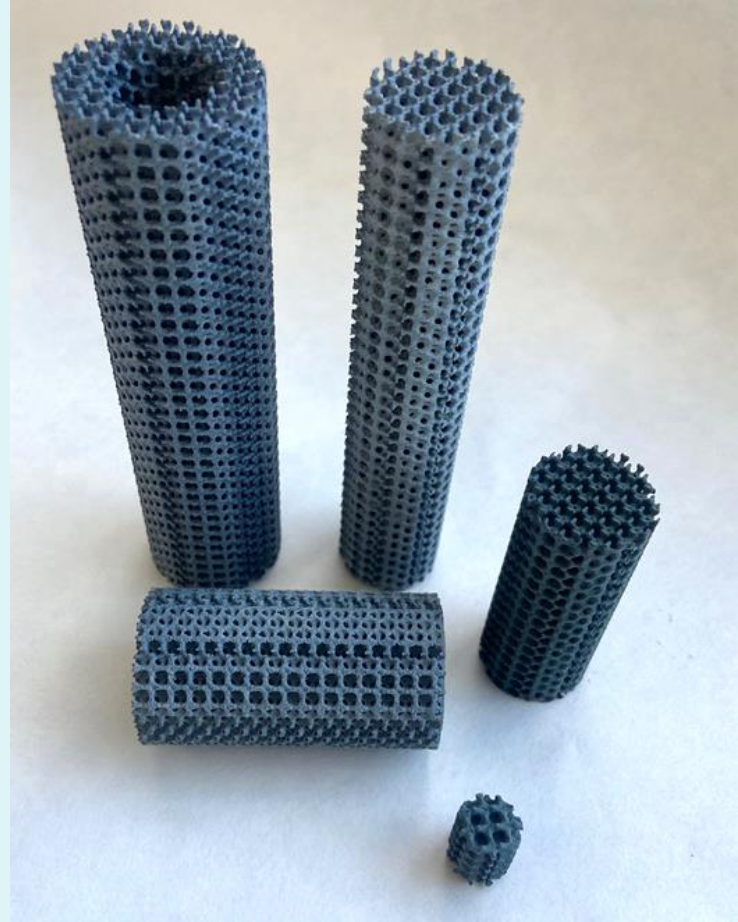
Dr. Antonio Vita



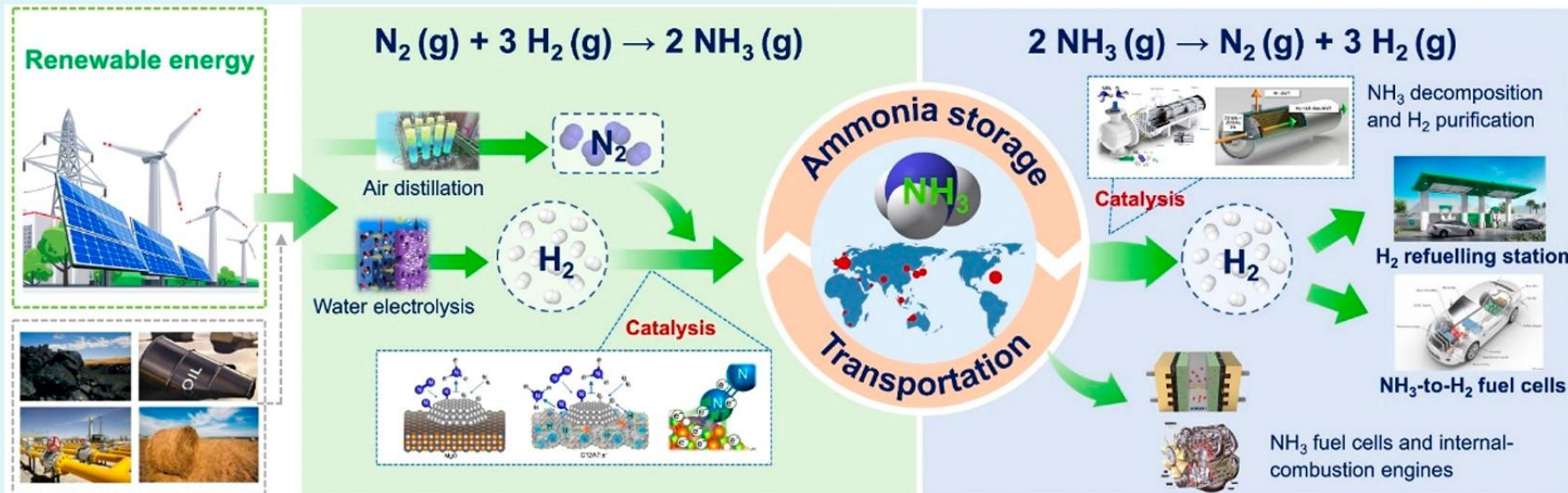
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98126 S. Lucia, Messina, Italy*

AMMONIA AS ENERGY CARRIER

Webinar
October 17rd 2024



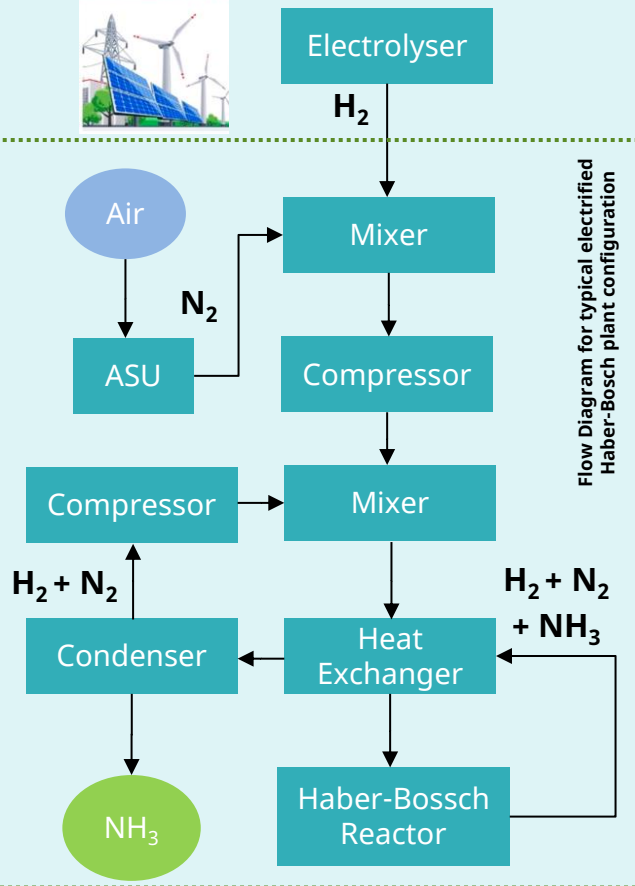
WHY AMMONIA?



AMMONIA AS ENERGY CARRIER VIA AMMONIA SYNTHESIS AND DECOMPOSITION

THE DECARBONISATION OF AMMONIA PRODUCTION

Green Ammonia production



- ### "Drawbacks"
- The capital expenditure for a green ammonia production plant is dominated by the electrolyzer cost

CAPEX, Haber-Bosch plant

183 M\$

CAPEX, alkaline electrolysis plant
486M\$

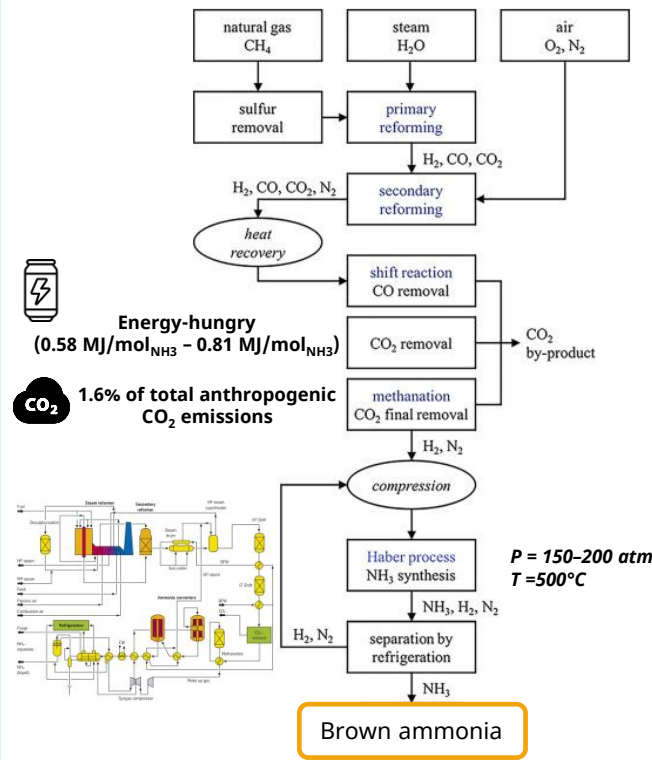
- The energy supply for green hydrogen feedstock is significantly greater than the electricity demand for the HB process.

35M W

Energy demand H₂ production (24/7)
374 MW

AMMONIA PRODUCTION ON A LARGE SCALE

Flow Diagram for the Multi-step Haber-Bosch Ammonia Production Process



- Daily production capacity: 1000 - 2200t
- Efficiency: 65%
- Gas velocities: 10000-20000 m³/m_{cat}.³h
- Typical conversions: 8-15%

THE DECARBONISATION OF AMMONIA PRODUCTION

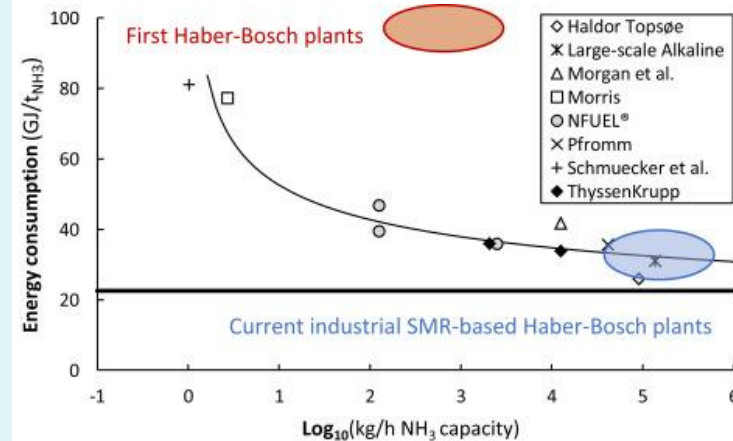
● Scale-Down and Intermittency issues

“Renewable sources of energy such as biomass, solar, wind or geothermal are characterized by a highly distributed production across regions”

- **Distributed production corresponds to the production at small scales**, for green ammonia production the step forward is **dawn-size of large-scale plant and modularization**;
- A large-scale ammonia plant ($\geq 1000 t_{NH_3}/d$) consumes about 2-7 GJ/ t_{NH_3} for pressurizing, heating, pumping and utilities;
- At intermediate scales (3-20 t_{NH_3}/d), this energy consumption increases to typically 13-14 GJ/ t_{NH_3} ;
- At very small scales ($< 0.1 t_{NH_3}/d$), heat is even required to keep the ammonia synthesis reactor at the synthesis temperature due to radial heat losses, and hydrogen and nitrogen production also becomes less efficient
- Intermittent **solar power and wind power cause variations in electricity supply**. Therefore, the synthesis loop should either be able to ramp up and down fast, or batteries should be installed to operate the synthesis loop at constant load

Energy consumption of various electrolysis-based Haber-Bosch processes (academic and industrial estimates).

The bold line represents the thermodynamic minimum energy consumption (22.5 GJ/ t_{NH_3})



$$E = (52.58 \cdot \log_{10}(\text{capacity in kg/h}))^{-0.30}$$

Upon scale-down, heat losses increase and the energy consumption increases

Milder operating conditions in the synthesis loop are required for effective scale-down

AMMONIA AND MOF BASED HYDROGEN STORAGE FOR EUROPE



WP3

“Key materials and components for long term Hydrogen Storage”

Task 3.3: Bench-scale (TRL 4) 3D printed POCS and novel JM catalysts:

Subtask 3.3.1: Design, manufacture and heat transfer performance characterization (under non-reactive conditions) of 3D printed POCS and commercial open cell foam [ENGIE, M1-M24]

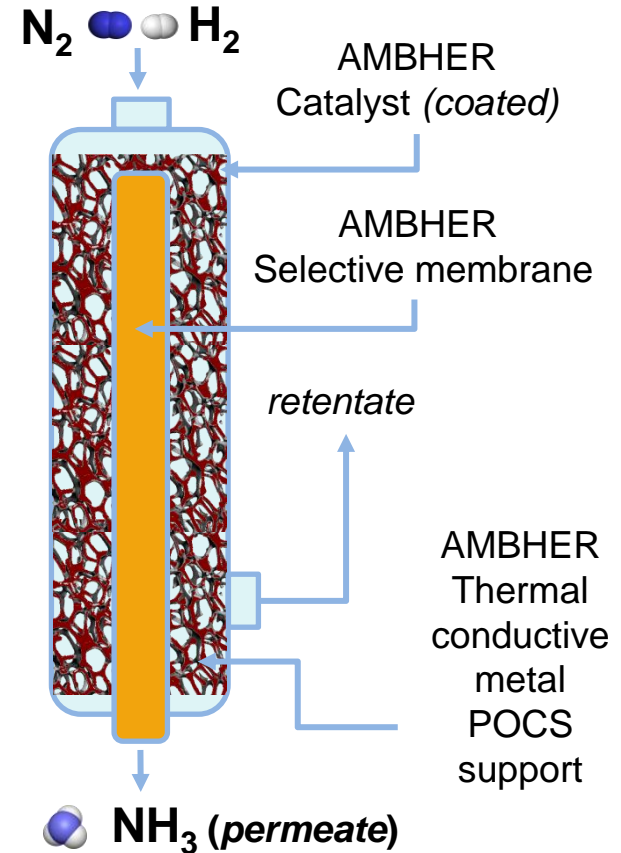
Subtask 3.3.2: Catalytic activation, characterization and performances of thermal conductive open-cell foams and POCS with commercial reference catalyst (1st generation) [CNR, ENGIE, M1-M24]

Subtask 3.3.3: Preparation and tests of novel Fe, Ru based catalysts [JM, M1-M24]

Subtask 3.3.4: Preparation of structured catalysts (2nd generation) for single CMR [CNR, ENGIE, TUE, M20-M24]

Subtask 3.5.2: Fabrication of structured catalysts (POCSs activated with novel catalyst) for single membrane reactor (TRL4) and the demonstrator plant (TRL5) [CNR, ENGIE, JM, M30-40]

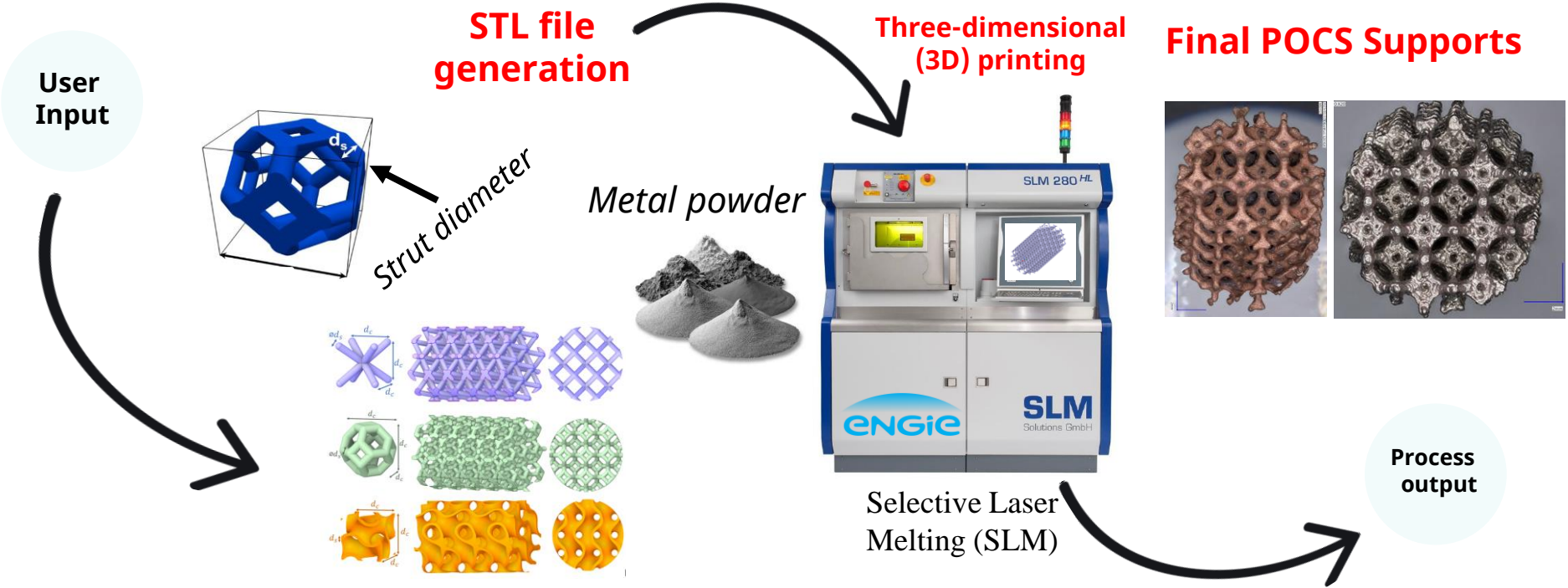
Integration POCS catalysts with membranes in a membrane reactor



Funded by
the European Union

Periodical Open Cellular Structures (POCS) 3D printed

❑ Schematic sequence of POCSs manufacturing process

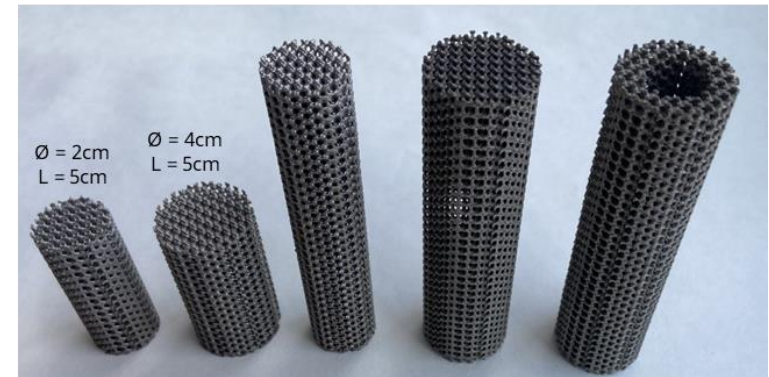
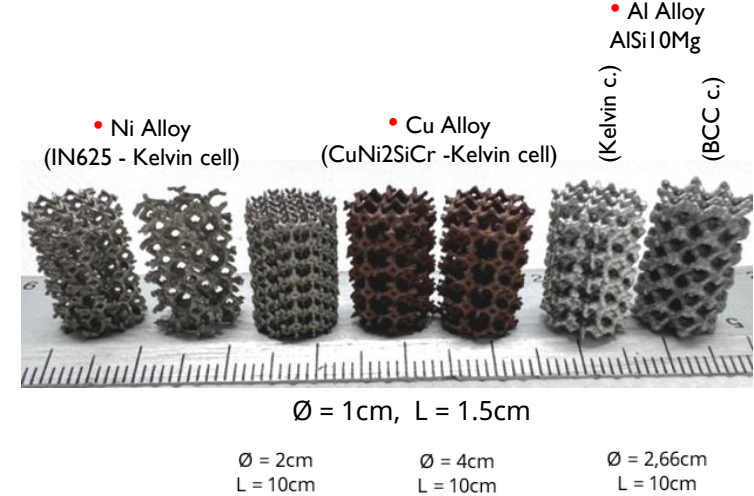


Detailed design with Netfabb software

Periodical Open Cellular Structures (POCS)

Material	Cell type	Cell size (mm)	Strut diameter (mm)	Volume (cm ³)	Surface (cm ²)	Surface/Volume ratio	Theor. Relative Density
Al alloy (AlSi10Mg)	BCC	3	0.6	0.220	12.94	58.82	0.17
	Kelvin	3	0.6	0.290	15.23	52.52	0.21
Cu alloy (CuNi2SiCr)	Kelvin	3	0.6	0.290	15.23	52.52	0.21

Material	Cell type	Cell size (mm)	Strut diameter (mm)	Volume (cm ³)	Surface (cm ²)	Surface/Volume ratio	Theor. Relative Density
Ni alloy (IN625)	Kelvin	3	0.6	0.290	15.23	52.52	0.21
		4	0.6	0.153	9.08	59.37	0.11
		3	0.8	0.518	16.93	32.68	0.36
		3	0.4	0.126	11.21	88.97	0.10
		1.5	0.3	0.292	29.79	102.02	0.23
		4	0.8	0.278	11.39	40.97	0.19
		2	0.4	0.288	22.46	78.00	0.22
		2	0.6	0.631	25.20	39.94	0.45

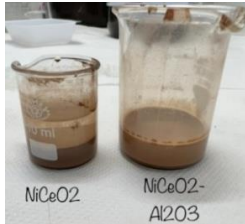


Scale-up strategy

Microscale studies

Influence of:

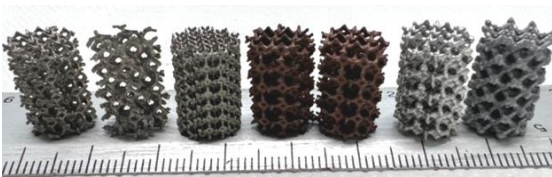
1. Slurry composition;
2. Catalyst formulation;
3. Powder ball milling rate;
4. Slurry ball milling time;
5. Support Thermal Treatment;
6. Support Anodization;
7. Primer (Disperal P2) utilization;
8. Support geometry (BCC, Kelvin);
9. Calcination temperature and time;
10. POCSs sand-blasted pretreatment;
11. Mechanical stability



Slurry composition

Glycerol	Water	Solid	PVA
42.5 %	33.6 %	22.4 %	1.5 %

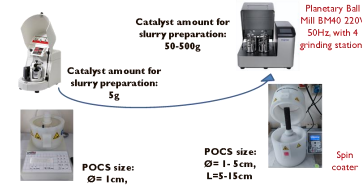
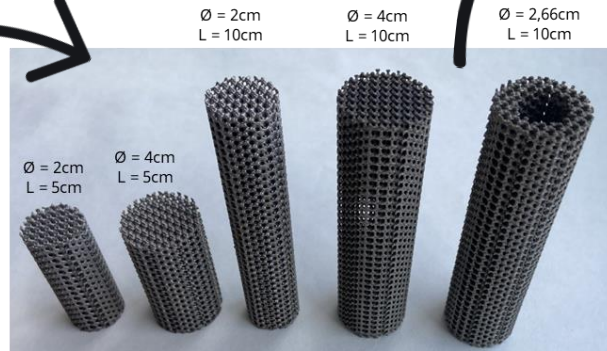
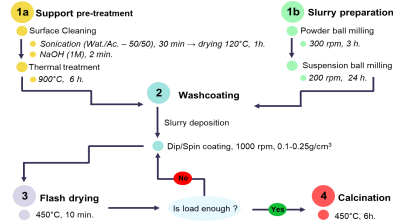
Ø = 1cm, L = 1.5cm



Intermediate scale-up

Influence of:

1. Slurry optimisation;
2. Coating process optimization;



Final scale-up for prototype

Influence of:

1. Equipment size;

Ø = 51cm, L = 10 - 20cm



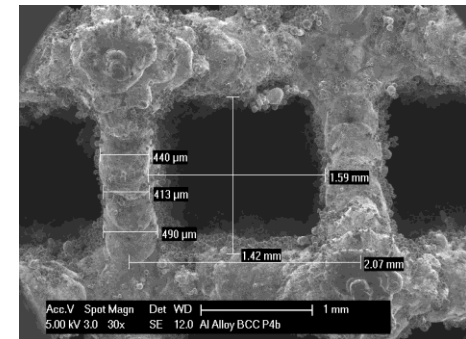
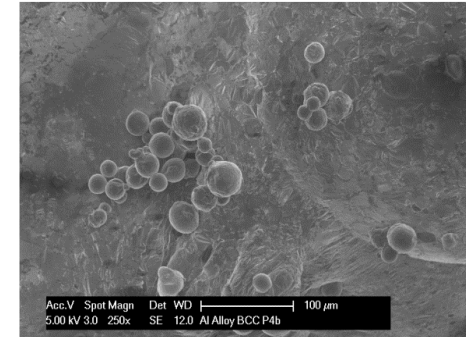
Morphological characterizations and porosity

Material	Cell type	Cell size (mm)	Strut diameter (mm)	** Solid Volume (cm ³)	** Solid density (g/cm ³)	Internal Surface area (cm ²)	** Porosity (%)	** Geom. density (g/cm ³)	Specific surf. area (cm ² /cm ³)	Relative density
IN625	BCC	2 (2*)	0.4 (0.41*)	0.219	10.87	9.45	82.9	2.80	87.03	0.17
IN625	BCC	2 (2*)	0.6 (0.6*)	0.489	8.79	24.52	63.9	2.02	48.77	0.36
IN625	BCC	3 (3*)	0.4 (0.4*)	0.099	11.31	19.06	92.1	3.65	95.66	0.08
IN625	BCC	3 (3*)	0.6 (0.59*)	0.220	8.86	23.85	83.3	0.95	58.82	0.17
IN625	BCC	3 (4*)	0.8 (0.75*)	0.395	4.41	9.47	71.5	1.66	39.01	0.29
IN625	BCC	4 (4*)	0.6 (0.62*)	0.116	9.14	12.94	91.2	1.48	64.48	0.09
IN625	BCC	4 (3*)	0.8 (0.75*)	0.206	16.02	15.41	85.2	0.90	45.85	0.15
IN625	BCC	1.5(1.5*)	0.3 (0.3*)	0.212	12.08	7.48	83.3	2.80	115.66	0.17



Elium pycnometer (Model I305 Multivolume, Micromeritics)

SEM micrographs

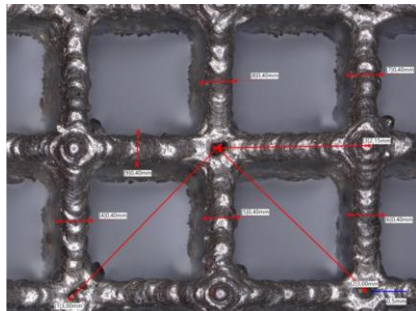


Measured value: *Calculated from optical images, **Calculated from He pycnometer measurement

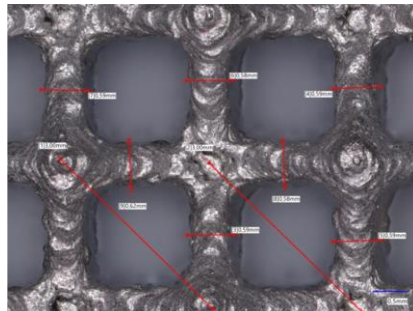
Ø = 1cm, L = 1.5cm

Optical microscope images of as-built BCC Ni-alloy POCS

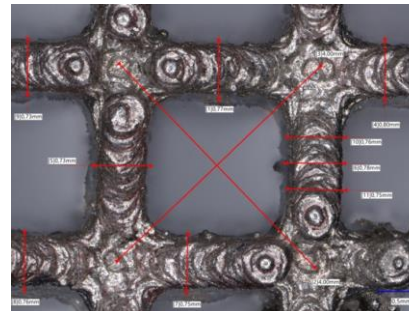
Cell Type = 3, Ø Strut = 0.4mm, SSA = 95.66 cm²/cm³, Porosity = 92%



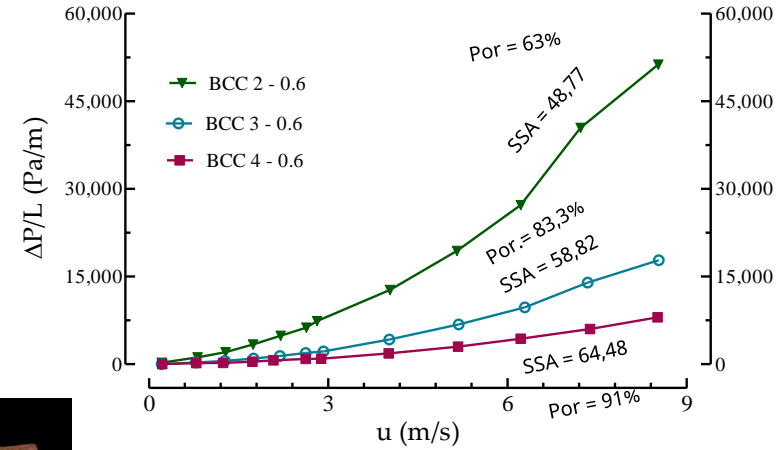
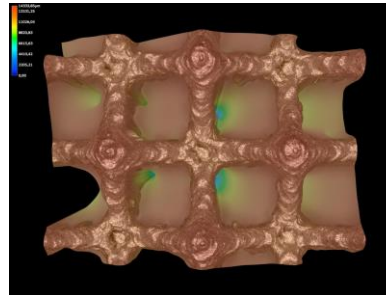
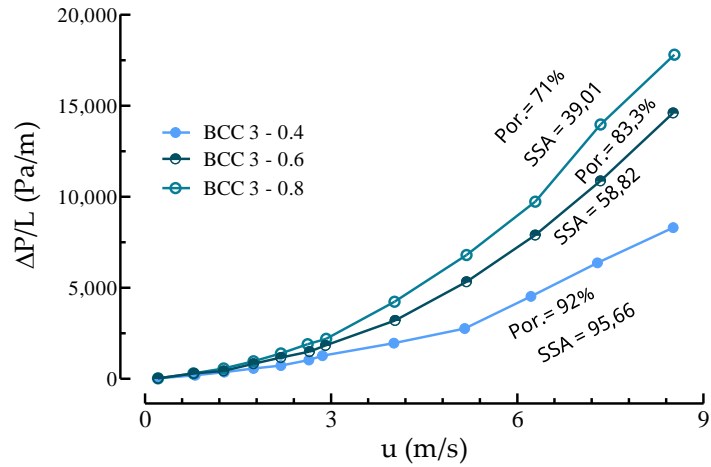
Cell Type = 3, Ø Strut = 0.6 mm, SSA = 58.82 cm²/cm³, Porosity = 83.3%



Cell Type = 3, Ø Strut = 0.8 mm, SSA = 39.01 cm²/cm³, Porosity = 71.3%



Pressure drop



Morphological characterizations and porosity

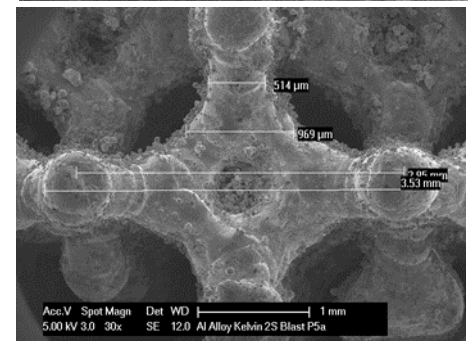
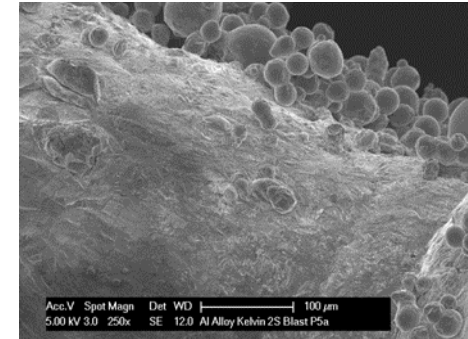
Material	Cell type	Cell size (mm)	Strut diameter (mm)	**Solid Volume (cm ³)	**Solid density (g/cm ³)	Internal Surface area (cm ²)	** Porosity (%)	** Geom. density (g/cm ³)	Specific surf. area (cm ² /cm ³)	Relative density
IN625	KELVIN	2 (2*)	0.6 (0.4*)	0.631	9.30	25.20	54.5	4.99	39.94	54.5
IN625	KELVIN	3 (3.04*)	0.4 (0.44*)	0.126	14.21	11.21	90.4	1.52	88.97	90.4
IN625	KELVIN	3 (3*)	0.6 (0.69*)	0.290	10.14	15.23	78.7	2.50	52.52	78.7
IN625	KELVIN	3 (3*)	0.8 (0.86*)	0.518	9.42	16.93	64.4	4.14	32.68	64.4
IN625	KELVIN	4 (4*)	0.6 (0.61*)	0.153	10.85	9.08	88.6	1.41	59.37	88.6



Elium pycnometer (Model 1305 Multivolume, Micromeritics)

Measured value: *Calculated from optical images, **Calculated from He pycnometer measurement $\varnothing = 1\text{cm}$, $L = 1.5\text{cm}$

SEM micrographs

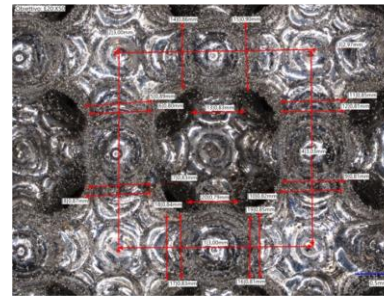
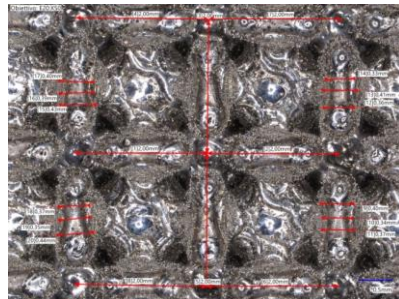
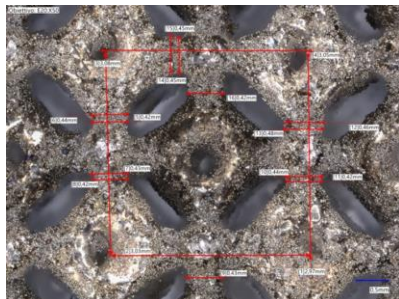


Optical microscope images of as-built kelvin Ni-alloy POCS

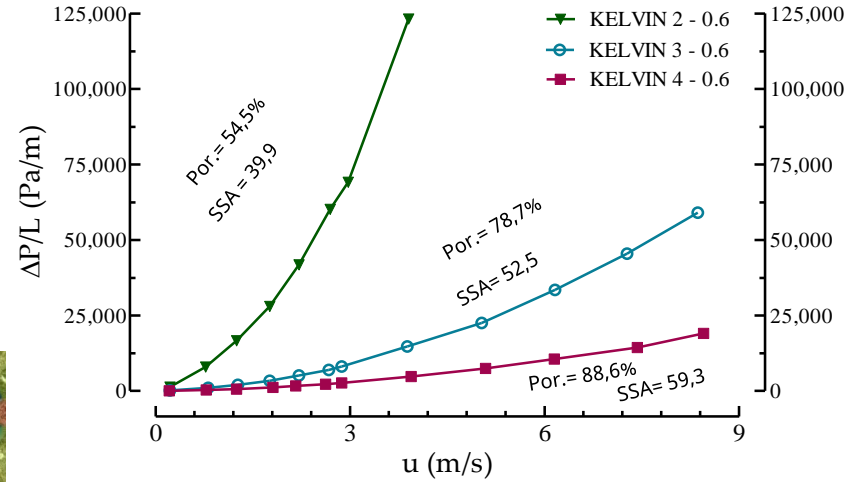
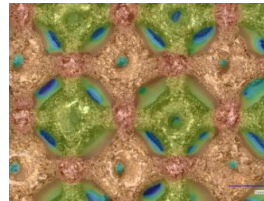
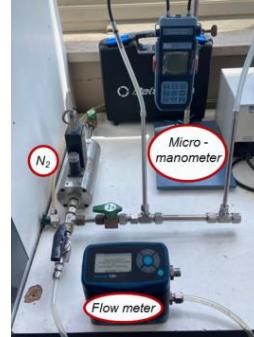
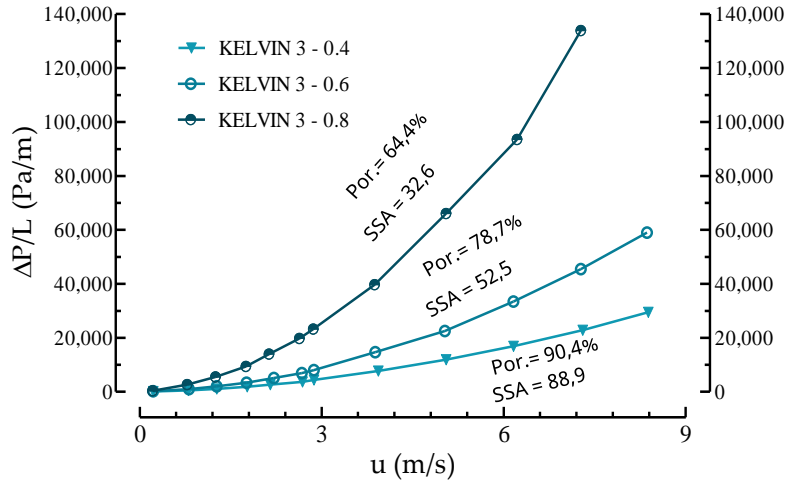
Cell Type = 3, \varnothing Strut = 0.4mm, SSA = 88.9 cm²/cm³, Porosity = 90.4%

Cell Type = 3, \varnothing Strut = 0.6 mm, SSA = 52,52 cm²/cm³, Porosity = 78,7%

Cell Type = 3, \varnothing Strut = 0.8 mm, SSA = 32,68 cm²/cm³, Porosity = 64.4%



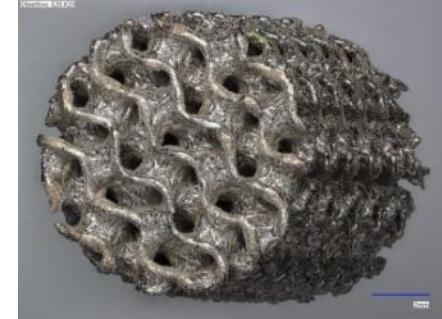
Pressure drop



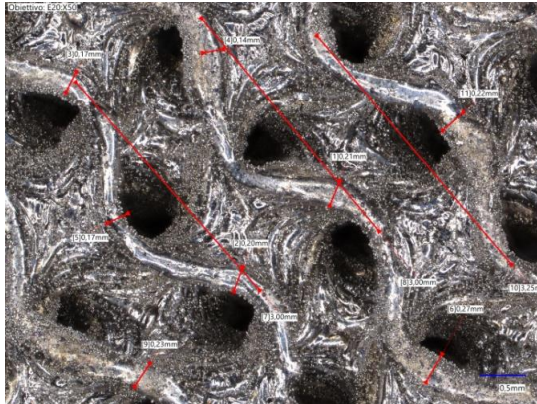
□ Morphological characterizations and porosity

$\varnothing = 1\text{cm}$, $L = 1.5\text{cm}$

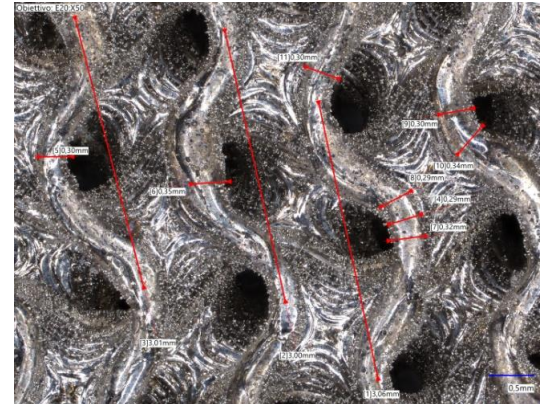
- Optical microscope images of as-built **GIROYD** Ni-alloy Triply Periodic Minimal Surface (TPMS) structure



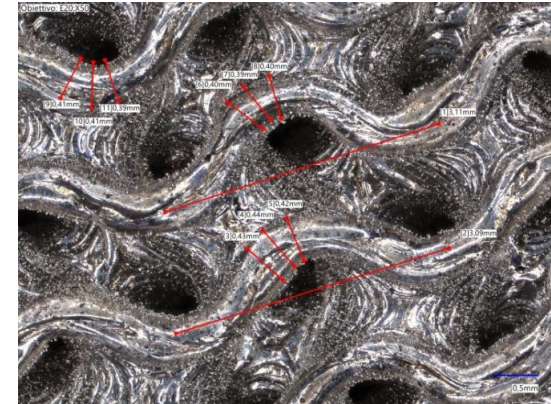
Cell Type = 3, \varnothing Strut = 0.23mm,
SSA = 20.4 cm²/cm³, Porosity = 79%



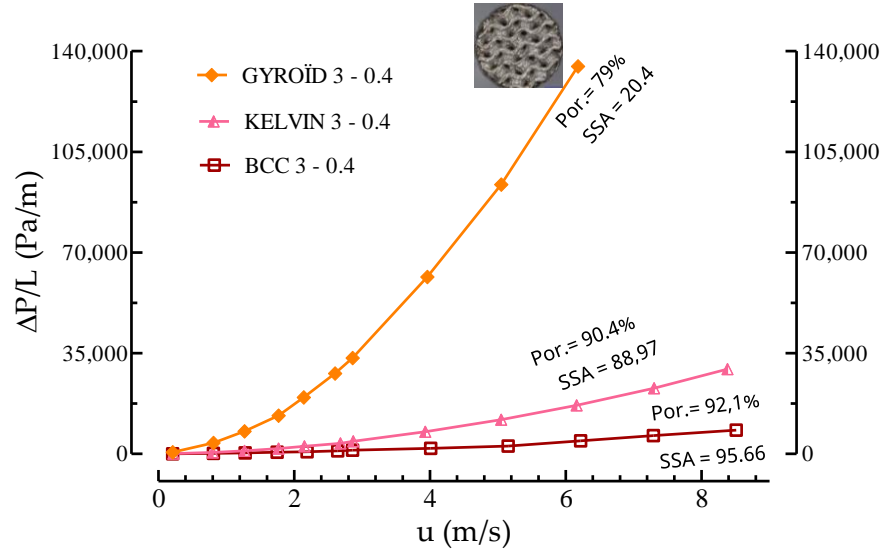
Cell Type = 3, \varnothing Strut = 0,3 mm,
SSA = 20,1 cm²/cm³, Porosity = 69,4%



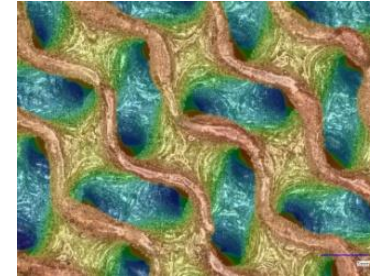
Cell Type = 3, \varnothing Strut = 0,4 mm,
SSA = 19.5 cm²/cm³, Porosity = 61%



Pressure drop (comparison Gyroid, Kelvin, BCC)

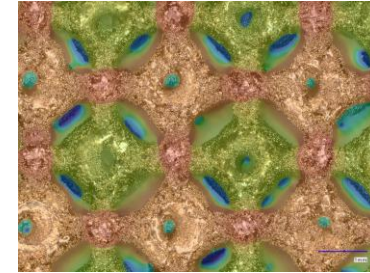


GYROID



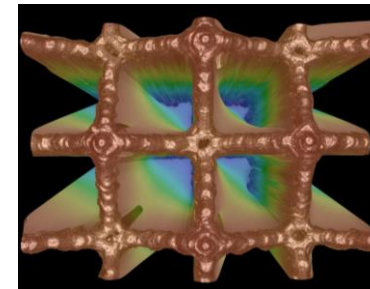
Cell Type = 3,
 \varnothing Strut = 0.4mm,
 SSA = 20.4 cm²/cm³,
 Porosity = 79%

KELVIN



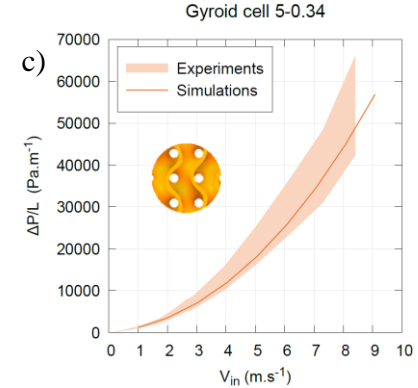
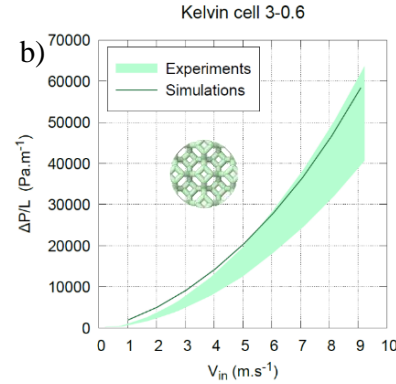
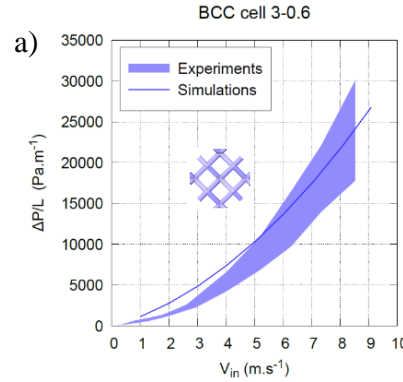
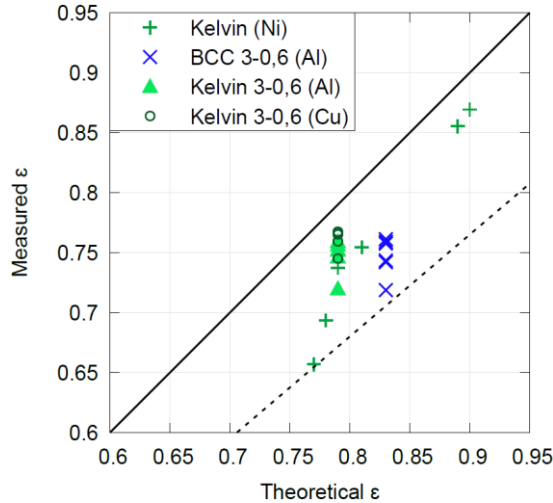
Cell Type = 3,
 \varnothing Strut = 0,4 mm,
 SSA = 88,97 cm²/cm³,
 Porosity = 90,4%

BCC



Cell Type = 3,
 \varnothing Strut = 0,4 mm,
 SSA = 95,66 cm²/cm³,
 Porosity = 92,1%

Experimental validation of CFD model a) BCC b) Kelvin c) Gyroid



Pressure drop comparison on various structures

Comparison of experimental hydrodynamic porosity vs. theoretical porosity. The 15% error margin is indicated by a dashed line.

**The printed samples
closely resemble their
CAD counterparts**

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Comparison of thermo-hydraulic performance among different 3D printed periodic open cellular structures

S. Richard^{a,*,1}, D. Tasso^b, M. Rajana^a, A. Saket^b, A. Ramirez Santos^b, C. Makhloufi^a, N. Meynet^a, B. Hary^b, S. Nardone^c, G. Marino^c, M. Thomas^c, C. Italiano^c, A. Vita^c, F. Gallucci^d

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^b ENGIE Laborélec, Rodestraat 125, 1630 Lukebeek, Belgium

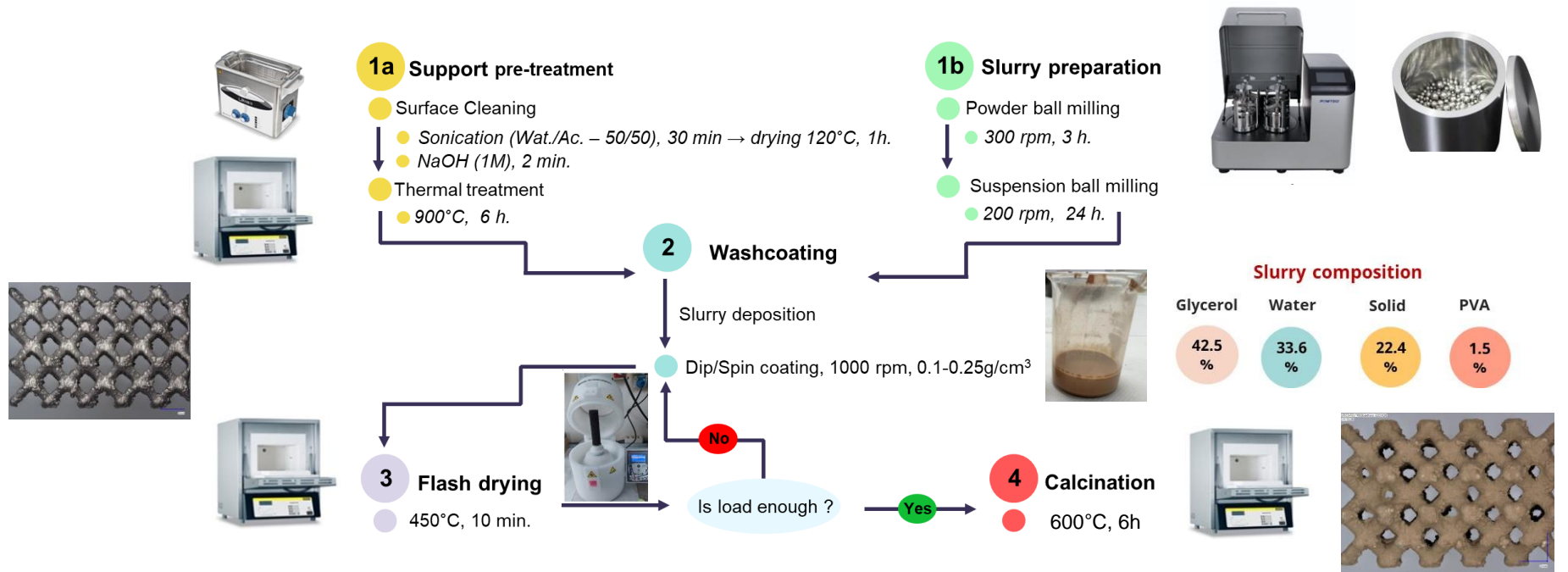
^c CNR-ITAE, Via Solito S. Lucia sopra Contesse n.5, S. Lucia, 98126 Messina, Italy

^d Sustainable Process Engineering, Chemical Engineering and Chemistry, Eindhoven University of Technology, Den Dolech 2, 5612 AZ, Eindhoven, the Netherlands



ACTIVATION OF NI-ALLOY POCS BY COMBINED DIP/SPIN COATING METHOD

Optimized dip/spin coating method



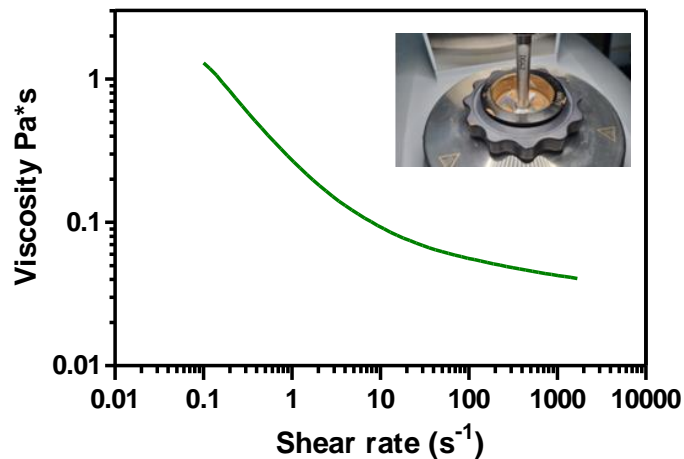
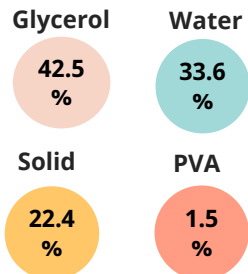
Main steps involved in the preparation of structured catalysts by washcoating

CATALYTIC ACTIVATION OF NI-ALLOY STRUCTURED SUPPORTS

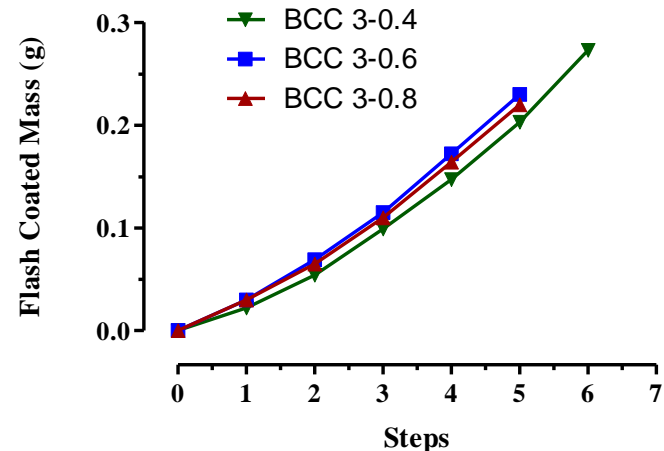
□ Activation of **Ni-Alloy POCS** and **TPMS** by combined dip/spin coating method

Slurry preparation with a 5wt%Ru/Al₂O₃ catalyst for the activation of KELVIN, BCC and GYROID structures

Slurry Composition



Rheological behaviour of slurry formulation (flow curve)



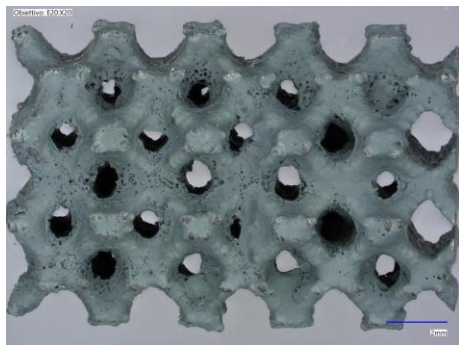
Loading curves

	Catalyst (g)	PVA (g)	Glycerol (g)	Water (g)	Ethanol (g)	No. Balls (1cm)	Volume of slurry (ml)
Batch 1	5	0.34	9.5	7.5	2	7	~16

CATALYTIC ACTIVATION OF NI-ALLOY STRUCTURED SUPPORTS

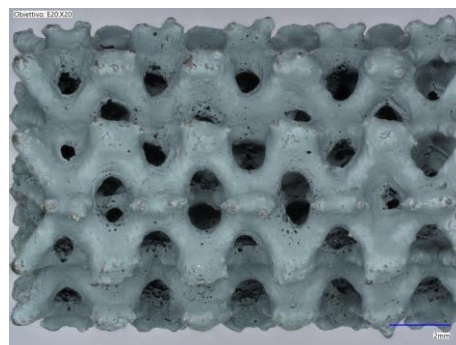
Coating of **BCC Ni-Alloy** POCS with a commercial 5wt% Ru/Al₂O₃ catalyst

Cat. loading: 0,272g
(0.23 g/cm³, 0.014g/cm²)



Cell Type = 3, Ø Strut = 0,4 mm,
SSA = 95,66 cm²/cm³,
Porosity = 86,17%

Cat. loading: 0,232
(0.19 g/cm³, 0.012 g/cm²)



Cell Type = 3, Ø Strut = 0,6 mm,
SSA = 58,82 cm²/cm³,
Porosity = 75,89%

Cat. loading: 0,241
(0.20 g/cm³, 0.015g/cm²)



Cell Type = 3, Ø Strut = 0,8 mm,
SSA = 39,01 cm²/cm³,
Porosity = 66.61%

Ø = 1cm, L = 1.5cm

Slurry Composition

Glycerol Water

42.5
%

33.6
%

Solid

PVA

22.4
%

1.5
%

$$\text{Catalyst Thickness} = \frac{m_{\text{catalyst}}}{\text{SSA}_{\text{POCS}} \times V_{\text{POCS}} \times d_{\text{layer}}}$$

POCS type	Cell size (mm)	Strut diameter (mm)	Solid Volume (cm ³)	Surface (cm ²)	Surface/Volume ratio (cm ² /cm ³)	Geometric V _{POCS} (cm ³)	Catalyst loaded (g)	Density cat. layer (g _{cat.} /cm ³)	Thickness (µm)
BCC	3	0,4	0,099	9,47	95,66	1,178	0,272	1,4	17,24
BCC	3	0,6	0,220	12,94	58,82	1,178	0,232	1,4	23,92
BCC	3	0,8	0,395	15,41	39,01	1,178	0,241	1,4	37,46

CATALYTIC ACTIVATION OF NI-ALLOY STRUCTURED SUPPORTS

Coating of **KELVIN Ni-Alloy** POCS with a commercial 5wt% Ru/Al₂O₃ catalyst

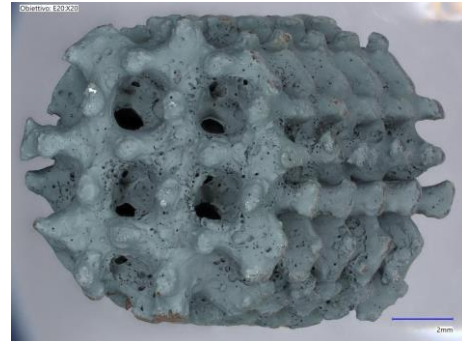
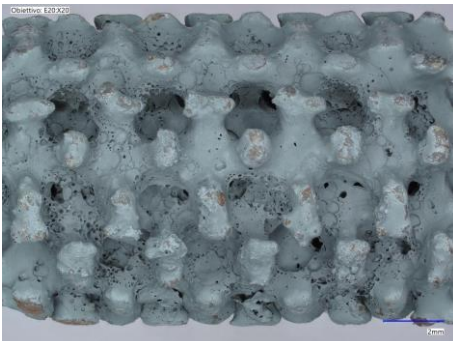
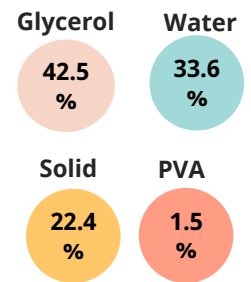
Cat. loading: 0,202g
(0.17 g/cm³, 0.014g/cm²)

Cat. loading: 0,234
(0.20 g/cm³, 0.012 g/cm²)

Cat. loading: 0,225
(0.19 g/cm³, 0.01g/cm²)

∅ = 1cm, L = 1.5cm

Slurry Composition



Cell Type = 3, ∅ Strut = 0,4 mm,
 SSA = 88,96 cm²/cm³,
 Porosity = 81,9%

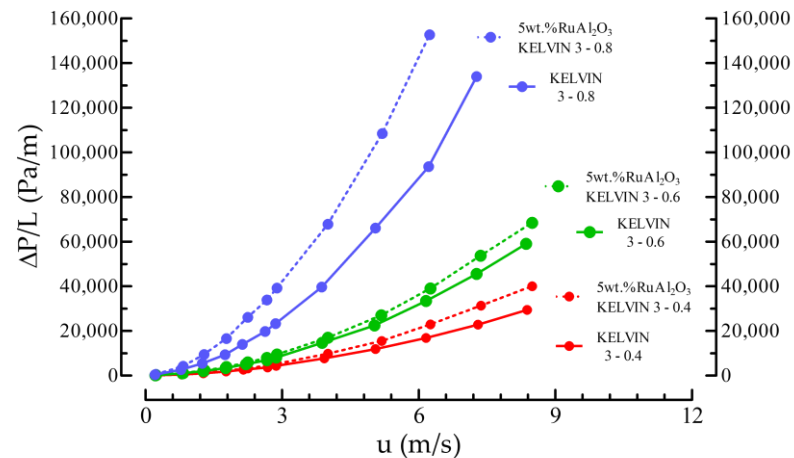
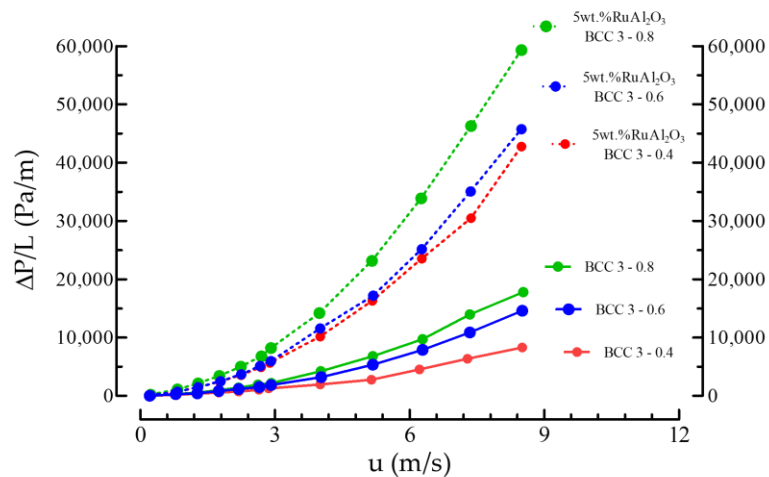
Cell Type = 3, ∅ Strut = 0,6 mm,
 SSA = 52,52 cm²/cm³,
 Porosity = 70,75%

Cell Type = 3, ∅ Strut = 0,8 mm,
 SSA = 32,68 cm²/cm³,
 Porosity = 51,54%

$$\text{Catalyst Thickness} = \frac{m_{\text{catalyst}}}{\text{SSA}_{\text{POCS}} \times V_{\text{POCS}} \times d_{\text{layer}}}$$

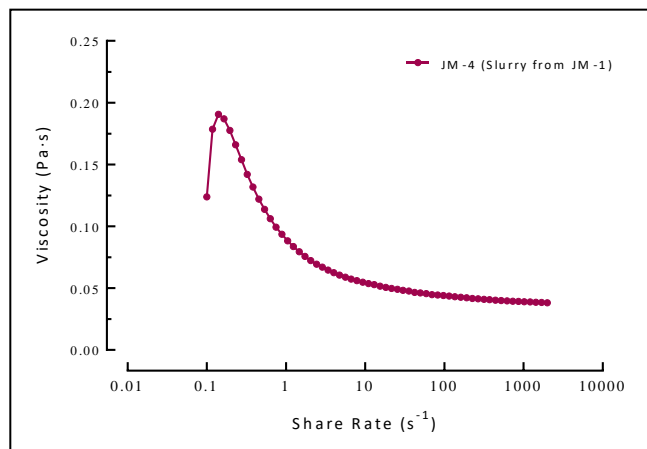
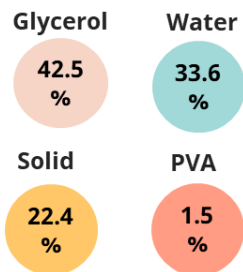
POCS type	Cell size (mm)	Strut diameter (mm)	Solid Volume (cm ³)	Surface (cm ²)	Surface/Volume ratio (cm ² /cm ³)	Geometric V _{POCS} (cm ³)	Catalyst loaded (g)	Density cat. layer (g _{cat.} /cm ³)	Thickness (µm)
Kelvin	3	0,4	0,126	11,21	88,97	1,178	0,202	1,4	13,77
Kelvin	3	0,6	0,290	15,23	52,52	1,178	0,234	1,4	27,02
Kelvin	3	0,8	0,518	16,93	32,68	1,178	0,225	1,4	41,74

□ Pressure drop (comparison Gyroid, Kelvin, BCC) influence of coating

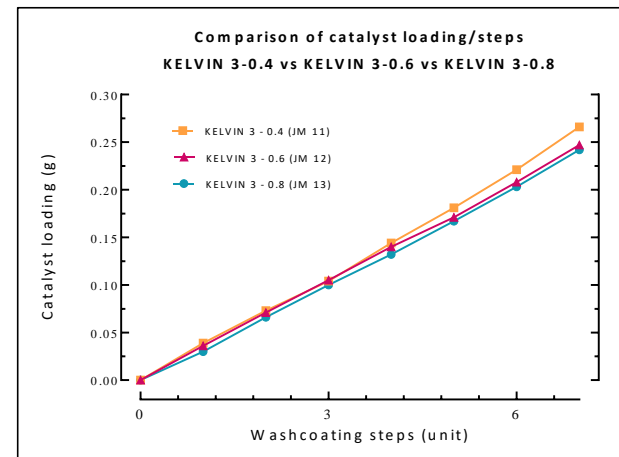


Slurry preparation with *novel JM catalyst (Ru-based)* for the activation of KELVIN, BCC and GYROD structures

Slurry Composition



Rheological behaviour of slurry formulation (flow curve)



Loading curves

	Catalyst (g)	PVA (g)	Glycerol (g)	Water (g)	Ethanol (g)	No. Balls (1cm)	Volume of slurry (ml)
Batch 1	5	0.34	9.5	7.5	2	7	~16

- Slurry preparation with **novel JM catalyst (Ru-based)** for the activation of **KELVIN**, and **BCC POCS**

$\varnothing = 1\text{cm}$, $L = 1.5\text{cm}$

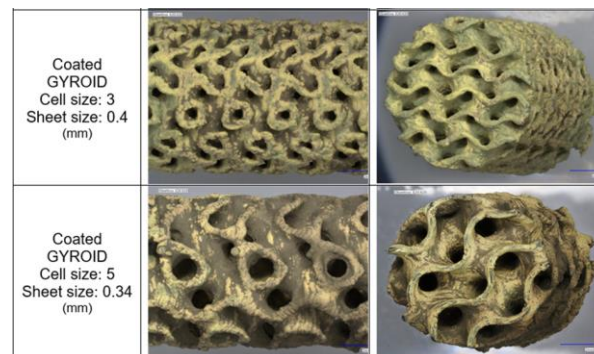
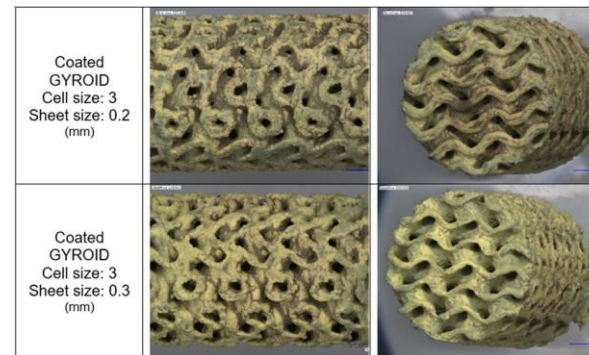
Support	Bare	Calcined	Washcoated	Calcined WC
KELVIN Cell size: 3 Strut size: 0.4 (mm)				
KELVIN Cell size: 3 Strut size: 0.6 (mm)				
KELVIN Cell: 3 Strut size: 0.8 (mm)				

Support	Bare	Calcined	Washcoated	Calcined WC
BCC Cell size: 3 Strut size: 0.4 (mm)				
BCC Cell size: 3 Strut size: 0.6 (mm)				
BCC Cell size: 3 Strut size: 0.8 (mm)				

- Slurry preparation with **novel JM catalyst (Ru-based)** for the activation of Triply Periodic Minimal Surface (TPMS) GYROID structures

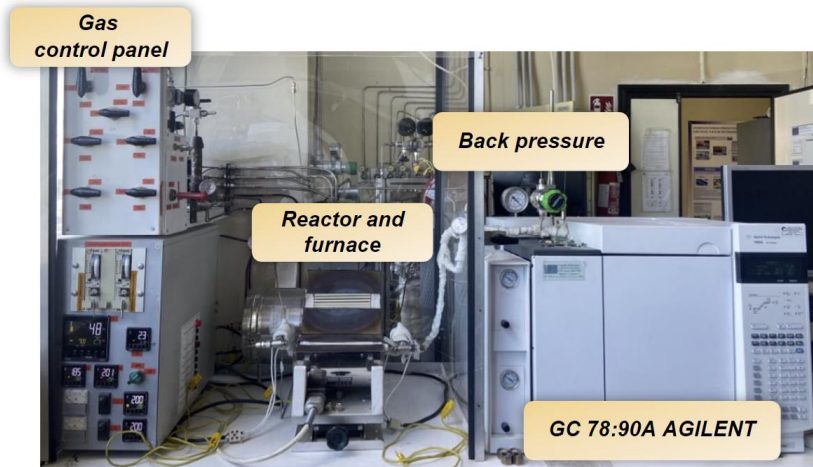
$\varnothing = 1\text{cm}$, $L = 1.5\text{cm}$

Support	Bare	Calcined	Washcoated	Calcined WC
GYROID Cell size: 3 Sheet size: 0.2 (mm)				
GYROID Cell size: 3 Sheet size: 0.3 (mm)				
GYROID Cell size: 3 Sheet size: 0.4 (mm)				
GYROID Cell size: 5 Sheet size: 0.34 (mm)				

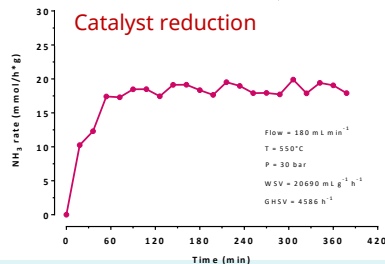


CATALYTIC ACTIVITY – AMMONIA SYNTHESIS

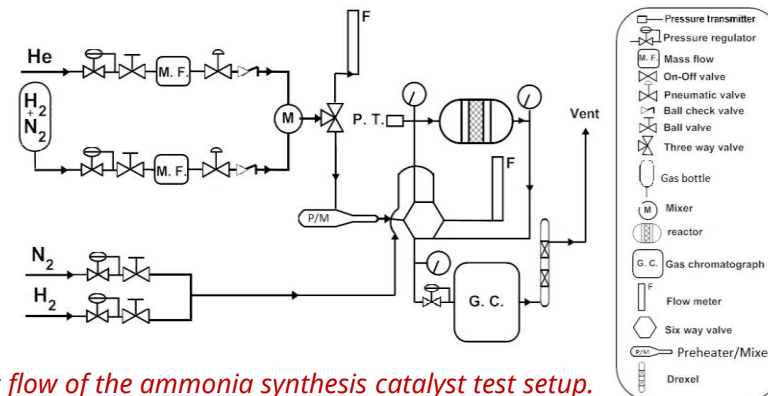
Catalytic activity (test set up)



Test rig for the evaluation of catalytic performances of catalysts towards the ammonia synthesis up to 50 bar



Operative conditions	
Temperature	300 - 550 (°C)
Pressure	20 (bar)
WSV	41379 (cm ³ g _{cat} ⁻¹ h ⁻¹)
GHSV	9172 (h ⁻¹)
Total IN Flow	90 - 540 cm ³ /min
H ₂ /N ₂	3:1 (H ₂ = 75%, N ₂ = 25%)
Catalyst	JM (Ru) -based AN5750



Schematic flow of the ammonia synthesis catalyst test setup.

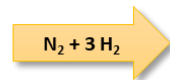
CATALYTIC ACTIVITY – AMMONIA SYNTHESIS

□ Catalytic tests at microscale with JM catalyst coated on POCS – Influence of geometry (KELVIN)


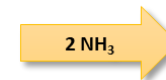
$\varnothing = 1\text{cm}$, $L = 1.5\text{cm}$

JM-11 (KELVIN 3-0.4)

Pressure (bar)	GHSV (h ⁻¹)	WSV (cm ³ g _{cat} ⁻¹ h ⁻¹)	Flow (mL/min)
20	9172	40602	180



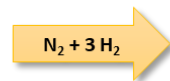
ξ_{cat}	Vol (cm ³)	g/cm ³
0.266	1,178	0,223


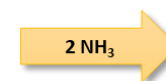
P = 20 bar					
χH_2			NH ₃ rate (mmol g ⁻¹ h ⁻¹)		
T 400	T 450	T 500	T 400	T 450	T 500
1.37	4.16	4.45	12.27	36.26	39.12

JM-12 (KELVIN 3-0.6)

Pressure (bar)	GHSV (h ⁻¹)	WSV (cm ³ g _{cat} ⁻¹ h ⁻¹)	Flow (mL/min)
20	9172	43725	180



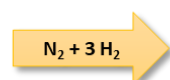
ξ_{cat}	Vol (cm ³)	g/cm ³
0.247	1,178	0,210


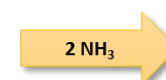
P = 20 bar					
χH_2			NH ₃ rate (mmol g ⁻¹ h ⁻¹)		
T 400	T 450	T 500	T 400	T 450	T 500
0.77	2.90	4.15	7.62	27.29	39.81

JM-13 (KELVIN 3-0.8)

Pressure (bar)	GHSV (h ⁻¹)	WSV (cm ³ g _{cat} ⁻¹ h ⁻¹)	Flow (mL/min)
20	9172	44628	180

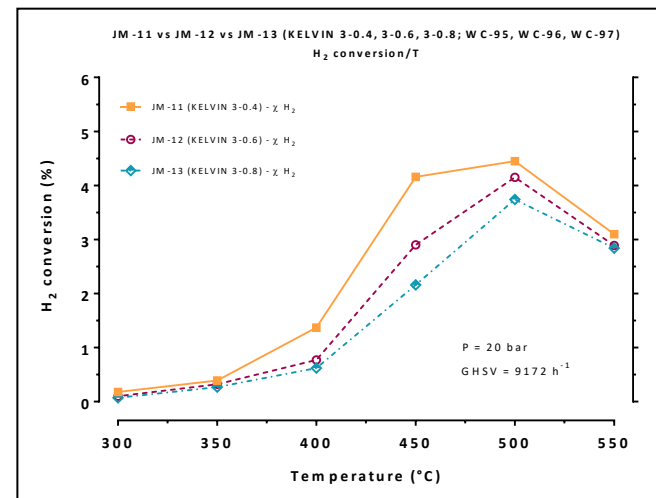
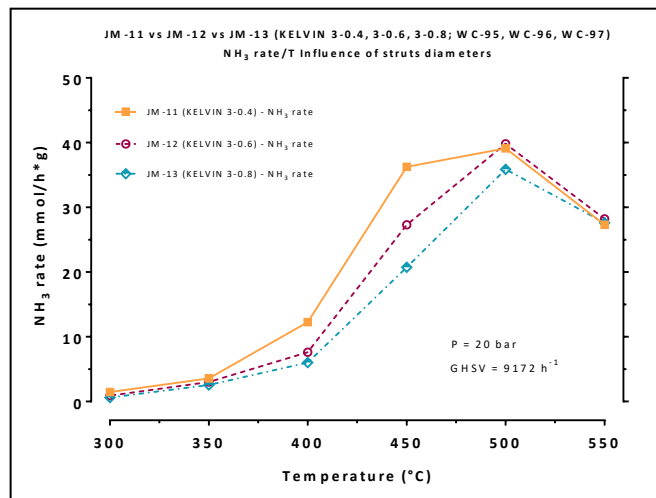


ξ_{cat}	Vol (cm ³)	g/cm ³
0.266	1,178	0,206

P = 20 bar					
χH_2			NH ₃ rate (mmol g ⁻¹ h ⁻¹)		
T 400	T 450	T 500	T 400	T 450	T 500
0.62	2.16	3.74	6.02	20.74	35.86

□ Catalytic tests at microscale with JM catalyst coated on POCS – Influence of geometry (KELVIN)



Coating	Cell type	Solid Volume (cm ³)	Solid Density (g/cm ³)	Porosity (%)	WC g _{cat} / V _{pyc} (g/cm ³)	Material	Cell type	Cell Size (mm)	Strut Diameter (mm)	Solid Volume (cm ³)	Solid Density (g/cm ³)	Internal Surface area (cm ²)	Porosity (%)	Geom. Density (g/cm ³)	Specific Surf. Area (cm ² /cm ³)	Relative density	WC g _{cat} / V _{geom}
JM-4	KELVIN 3-0.4	0.248**	8,2497**	78.91**	0.266 1.071**	ING25	KELVIN	3 (3.01*)	0.4 (0.42*)	0.126 (0.217**)	14.21 (8.2386**)	11.21	90.4 (81.94**)	1.52	88.97	0.10	0.266 0.226***
JM-4	KELVIN 3-0.6	0.382**	8,2924**	67.59**	0.247 0.647**	ING25	KELVIN	3 (3*)	0.6 (0.6*)	0.290 (0.350**)	10.14 (8.3484**)	15.23	78.7 (70.75**)	2.50	52.52	0.21	0.247 0.210***
JM-4	KELVIN 3-0.8	0.607**	8.4046**	48.46**	0.242 0.399**	ING25	KELVIN	3 (3*)	0.8 (0.81*)	0.518 (0.577**)	9.42 (8.4166**)	16.93	64.4 (51.64**)	4.14	32.68	0.36	0.242 0.206***

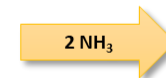
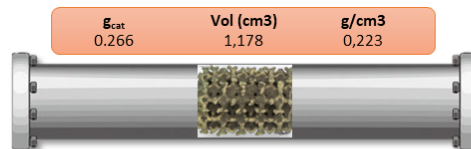
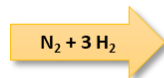
CATALYTIC ACTIVITY – AMMONIA SYNTHESIS

□ Catalytic tests at microscale with JM catalyst coated on POCS – Influence of geometry (KELVIN, BCC, GYROID)

$\varnothing = 1\text{cm}$, $L = 1.5\text{cm}$

JM-11 (KELVIN 3-0.4)

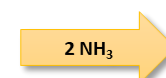
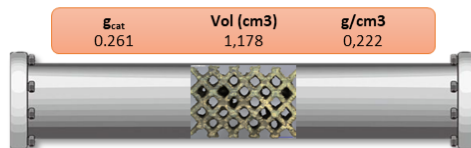
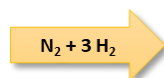
Pressure (bar)	GHSV (h ⁻¹)	WSV (cm ³ g _{cat} ⁻¹ h ⁻¹)	Flow (mL/min)
20	9172	40602	180



P = 20 bar					
χH_2			NH ₃ rate (mmol g ⁻¹ h ⁻¹)		
T 400	T 450	T 500	T 400	T 450	T 500
1.37	4.16	4.45	12.27	36.26	39.12

JM-14 (BCC 3-0.4)

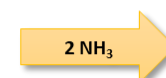
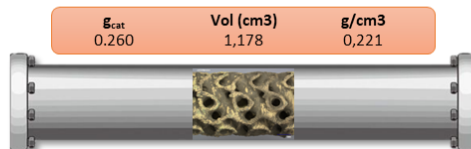
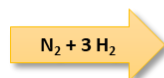
Pressure (bar)	GHSV (h ⁻¹)	WSV (cm ³ g _{cat} ⁻¹ h ⁻¹)	Flow (mL/min)
20	9172	41379	180



P = 20 bar					
χH_2			NH ₃ rate (mmol g ⁻¹ h ⁻¹)		
T 400	T 450	T 500	T 400	T 450	T 500
2.01	4.63	4.52	17.82	41.02	40.47

JM-24 (GYROID 5-0.34)

Pressure (bar)	GHSV (h ⁻¹)	WSV (cm ³ g _{cat} ⁻¹ h ⁻¹)	Flow (mL/min)
20	9172	41538	180



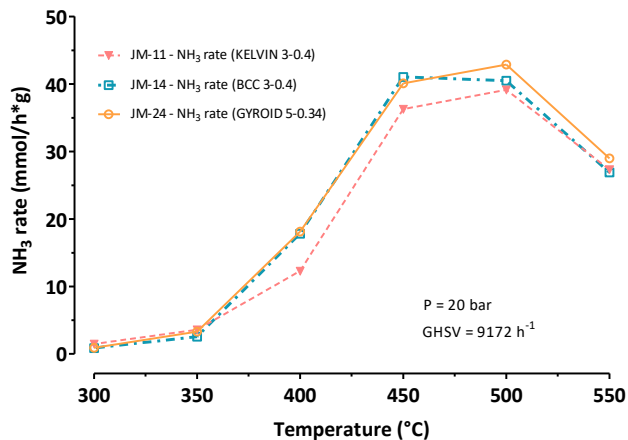
P = 20 bar					
χH_2			NH ₃ rate (mmol g ⁻¹ h ⁻¹)		
T 400	T 450	T 500	T 400	T 450	T 500
2.02	4.43	4.82	18.13	40.08	42.86

CATALYTIC ACTIVITY – AMMONIA SYNTHESIS

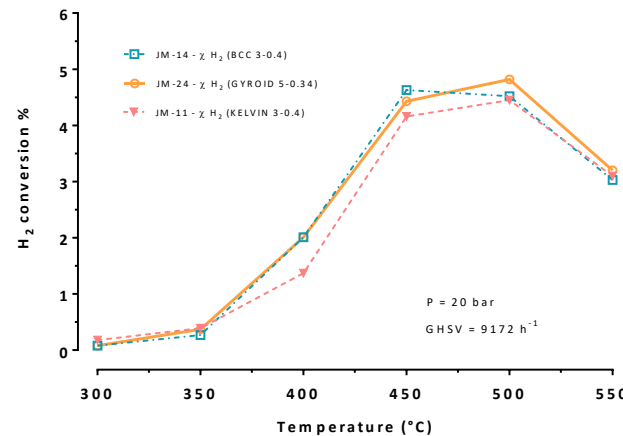


Catalytic tests at microscale with JM catalyst coated on POCS – Influence of geometry (KELVIN, BCC, GYROID)

JM-11 (KELVIN 3-0.4 WC-95) vs JM-14 (BCC 3-0.4 WC-98) vs JM-24 (GYROID 5-0.34 WC-107)
NH₃ rate/T Influence of geometry



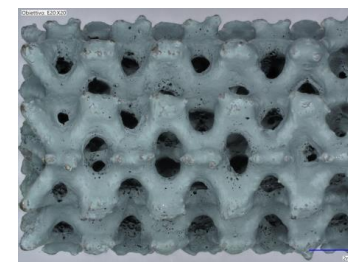
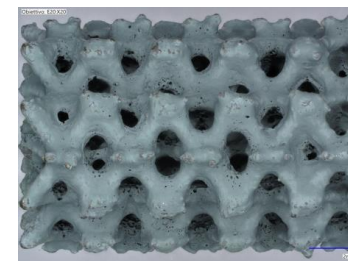
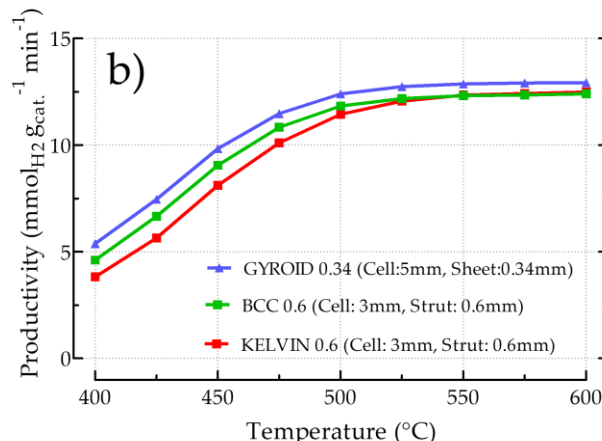
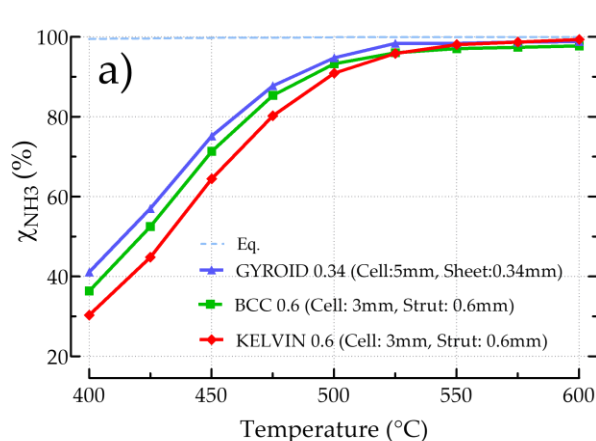
JM-11 (KELVIN 3-0.4 WC-95) vs JM-14 (BCC 3-0.4 WC-98) vs JM-24 (GYROID 5-0.34 WC-107)
H₂ conversion Influence of geometry



Coating	Cell type	Solid Volume (cm ³)	Solid Density (g/cm ³)	Porosity (%)	WC $\frac{\rho_{cat}}{\rho_{pyc}}$ (g/cm ³)
JM-4	KELVIN 3-0.4	0.248**	8,2497**	78.91**	0.266 1.071**
JM-4	BCC 3-0.4	0.165**	8,2134**	83.46**	0.261 1.071**
JM-4	GYROID 5-0.34	0.3577**	8.4203**	69.62**	0.260 0.727**

Material	Cell type	Cell Size (mm)	Strut Diameter (mm)	Solid Volume (cm ³)	Solid Density (g/cm ³)	Internal Surface area (cm ²)	Porosity (%)	Geom. Density (g/cm ³)	Specific Surf. Area (cm ² /cm ³)	Relative density	WC $\frac{\rho_{cat}}{\rho_{geom}}$
IN625	KELVIN	3 (3.01*)	0.4 (0.42*)	0.126 (0.217**)	14.21 (8.2386**)	11.21	90.4 (81.94**)	1.52	88.97	0.10	0.266 0.226***
IN625	BCC	3 (3*)	0.4 (0.4*)	0.099 (0.165**)	11.31 (8.213**)	19.06	92.1 (86.01**)	3.65	95.66	0.08	0.261 0.222***
IN625	GYROID	5 (5.18*)	0.34 (0.34*)	(0.325**)	(8.4966**)	14.51	(72.40**)	Not reported	59.22	0.791	0.260 0.221***

□ Catalytic tests at microscale with 5wt%Ru/CeO₂ – Influence of geometry (KELVIN, BCC, GYROID)

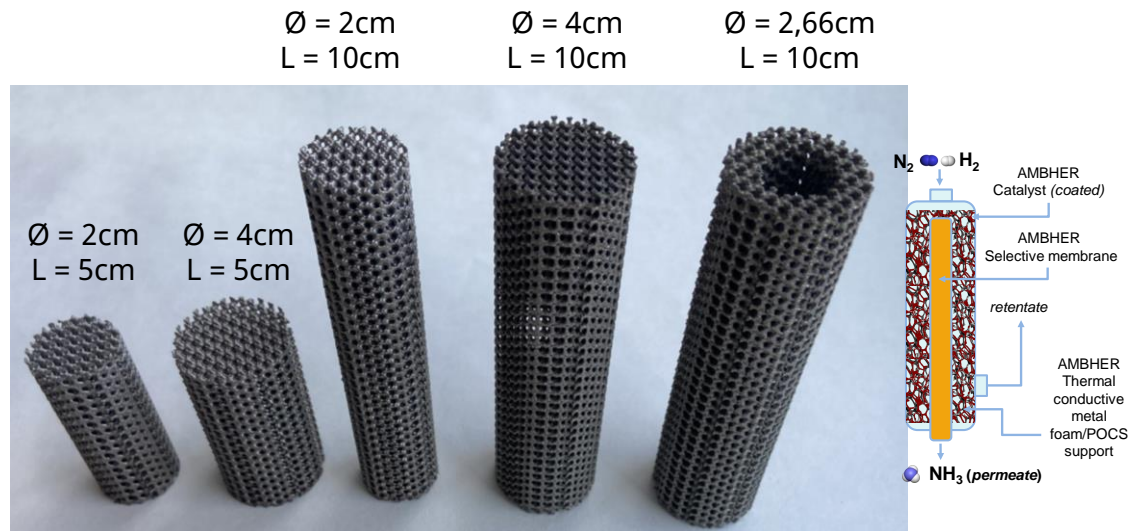
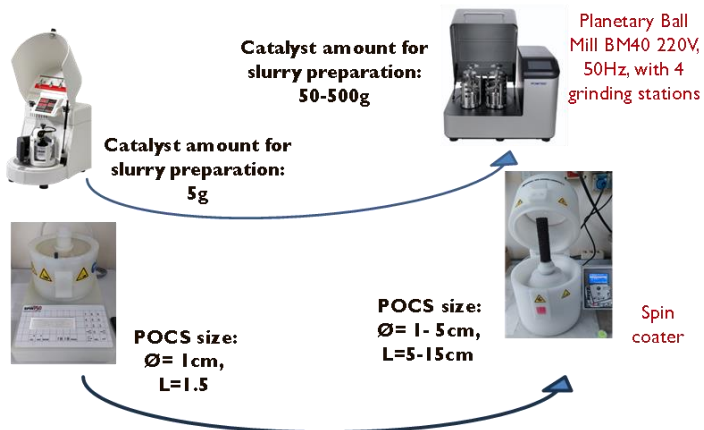


Performances of Ni-Alloy structures activated by 5wt%Ru/Al₂O₃, influence of Strut size (0.4, 0.34mm) and cell size (5, 3mm). GYROID 0.34: (Cell size = 5, catalyst loading = 0.225g, 0.19g/cm³, WSV = 27067cm³gcat-1 h⁻¹), BCC 0.6: (catalyst loading = 0.232g, 0.2g/cm³, WSV = 26250 cm³gcat-1 h⁻¹), KELVIN 0.6: (catalyst loading = 0.234g, 0.2g/cm³, WSV = 26154 cm³gcat-1 h⁻¹). Operating conditions: He = 54%vol., NH₃ = 46%vol., P = 1 bar, T = 400-600°C, total flow = 102 cm³ min⁻¹, GHSV = 5172 h⁻¹.

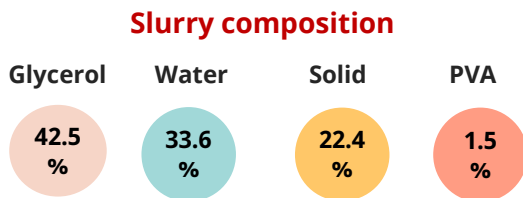
Cell type	Cell Size (mm)	Strut/sheet Size (mm)	Solid Volume (cm ³)	Solid Density (g/cm ³)	Internal Surface area (cm ²)	Porosity (%)	Surface/Solid Vol. (cm ² /cm ³)	Cat. Layer thickness (μm)
BCC 0.6	3	0.6	0.220	8.86	12.94	83.3	58.82	(23.92****)
	(3*)	(0.59*)	(0.284**)	(8.40**)		(75.89****)		
KELVIN 0.6	3	0.6	0.290	10.14	15.23	78.7	52.52	(27.02****)
	(3*)	(0.61*)	(0.344**)	(8.50**)		(70.75****)		
GYROID 0.34	5	0.34	0.245	11.26	14.51	79.2	59.22	(26.11****)
	(5.18*)	(0.34*)	(0.325**)	(8.49**)		(72.40****)		

SCALE UP OF STRUCTURED CATALYSTS

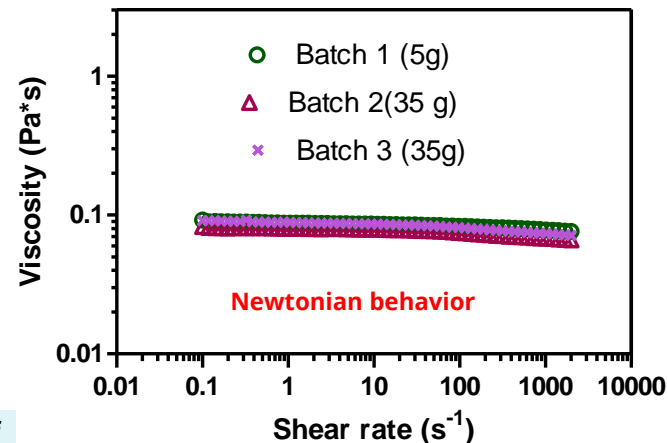
Scale-up of the dip/spin coating method (*second generation of POCS*)



Scale-up of the dip/spin coating method (*second generation of POCS*)



Catalyst:
Commercial
0.5wt%Ru/Al₂O₃



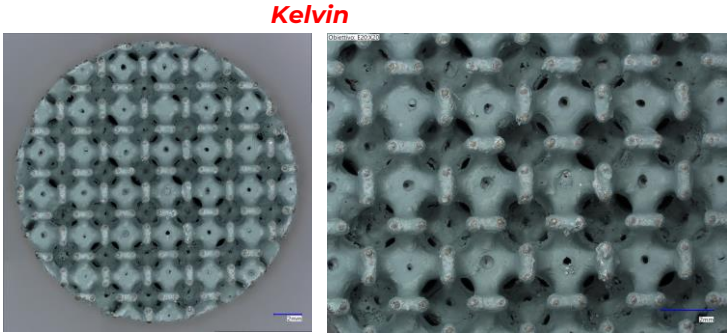
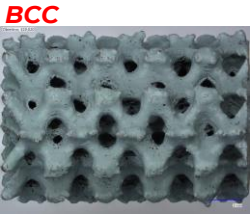
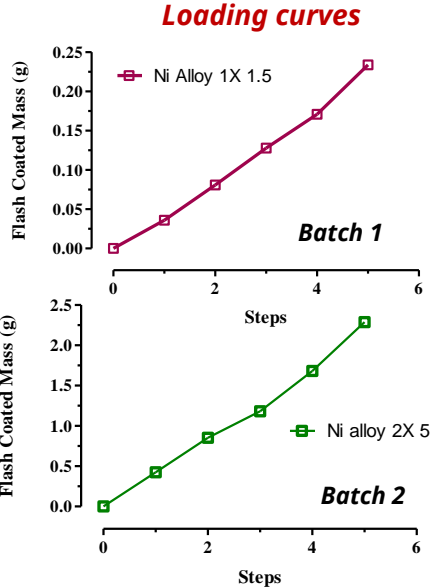
Rheological behaviour of slurry formulations (flow curves)

	Catalyst (g)	PVA (g)	Glycerol (g)	Water (g)	Ethanol (g)	No. Balls (1cm)	Volume of slurry (ml)
Batch 1	5	0.34	9.5	7.5	2	7	~16
Batch 2	10	0.68	19	15	4	14	~32
Batch 3	35	2.38	66.5	52.5	14	50	~155

Batch 2 and 3 were used for coating large supports

SCALE UP OF STRUCTURED CATALYSTS

Scale-up of the dip/spin coating method



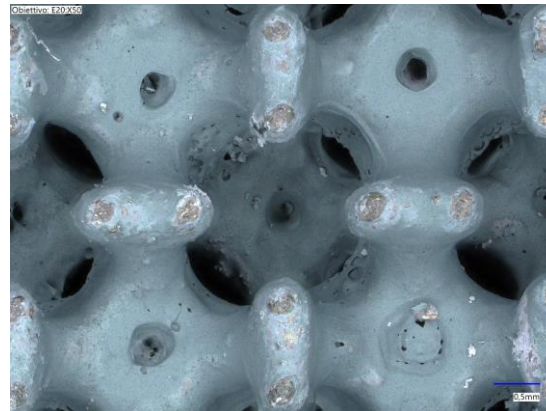
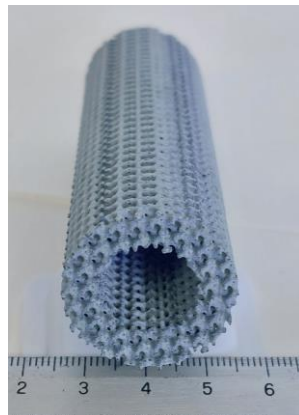
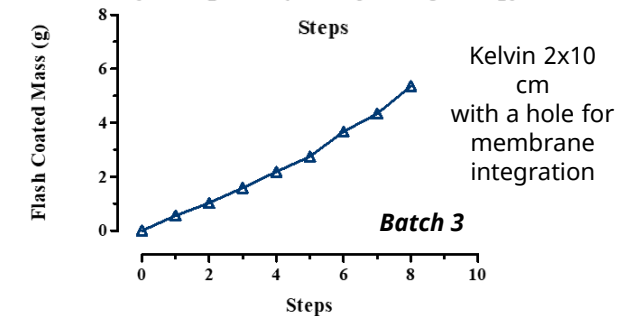
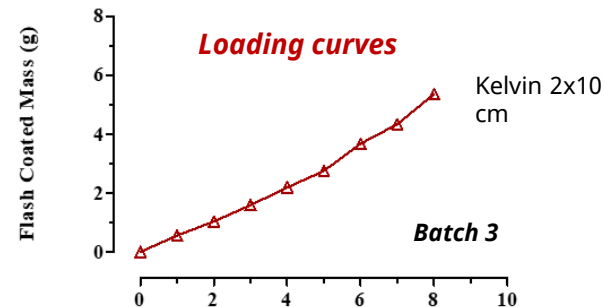
Catalyst: Commercial 0.5wt% Ru/Al₂O₃

	Catalyst (g)	PVA (g)	Glycerol (g)	Water (g)	Ethanol (g)	No. Balls (1cm)	Volume of slurry (ml)
Batch 1	5	0.34	9.5	7.5	2	7	~16
Batch 2	10	0.68	19	15	4	14	~32
Batch 3	35	2.38	66.5	52.5	14	50	~155

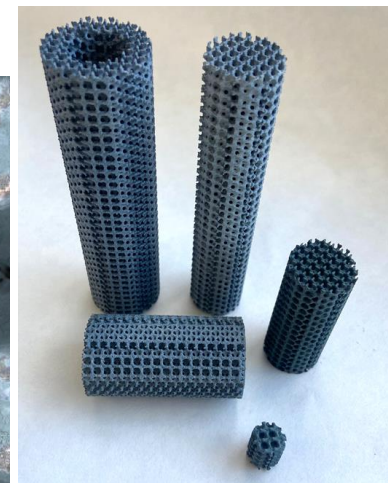


Scale-up of the dip/spin coating method (*second generation of POCS*)

Catalyst: Commercial 0.5wt% Ru/Al₂O₃

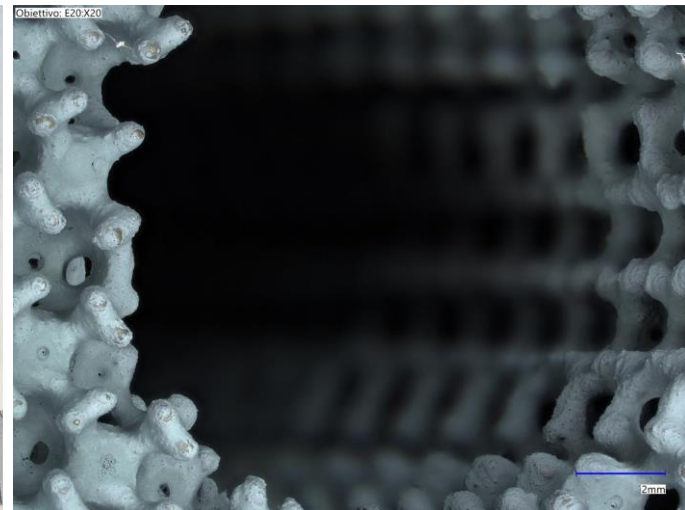
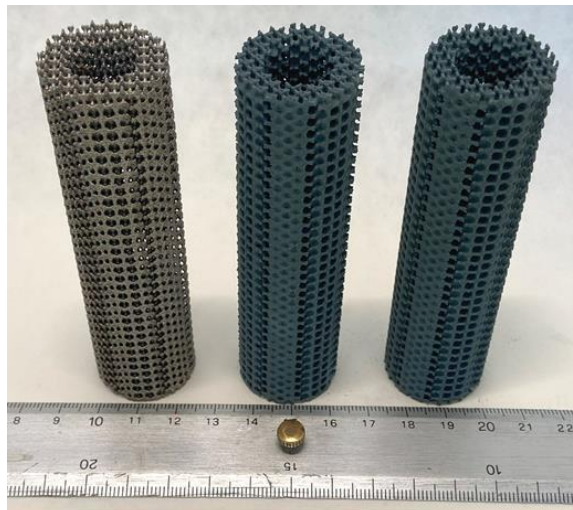
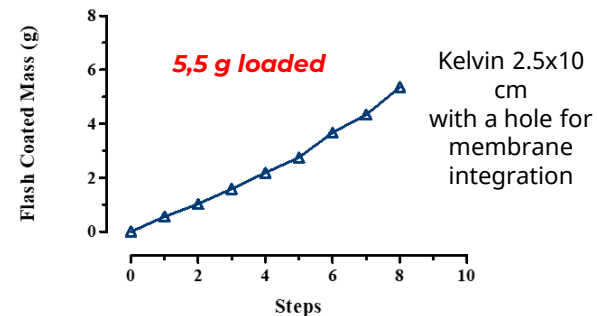


	Catalyst (g)	PVA (g)	Glycerol (g)	Water (g)	Ethanol (g)	No. Balls (1cm)	Volume of slurry (ml)
Batch 1	5	0.34	9.5	7.5	2	7	~16
Batch 2	10	0.68	19	15	4	14	~32
Batch 3	35	2.38	66.5	52.5	14	50	~155

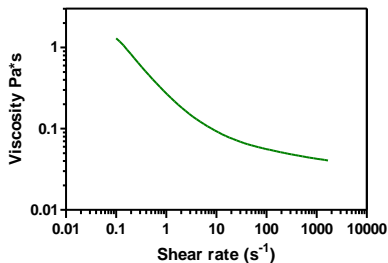
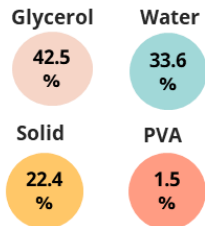


Scale-up of the dip/spin coating method (*second generation of POCS*)

Catalyst: Commercial 5wt% Ru/Al₂O₃



Slurry Composition

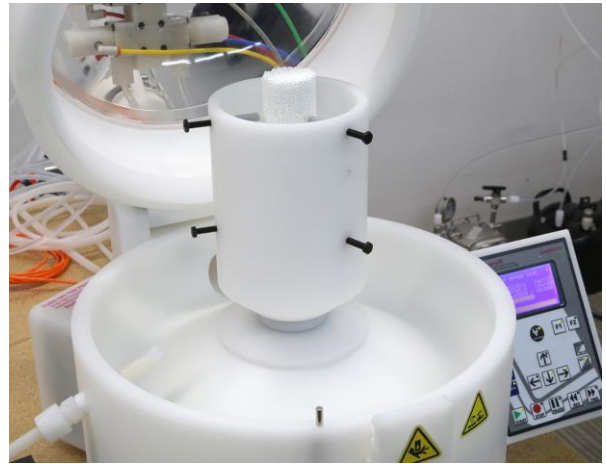
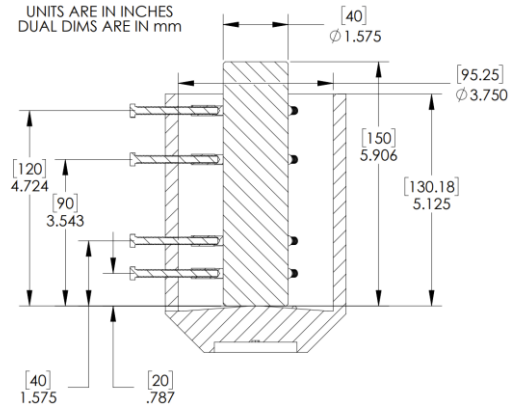


Rheological behaviour of slurry formulation (flow curve)

	Catalyst (g)	PVA (g)	Glycerol (g)	Water (g)	Ethanol (g)	No. Balls (1cm)	Volume of slurry (ml)
Batch 3	35	2.38	66.5	52.5	14	50	~155

SCALE UP OF STRUCTURED CATALYSTS

- Scale-up of the dip/spin coating method (**third generation of BCC and GYROID**)
- Design and realization of a new specimen holder for the spin-coater to host supports with size for the demonstrator



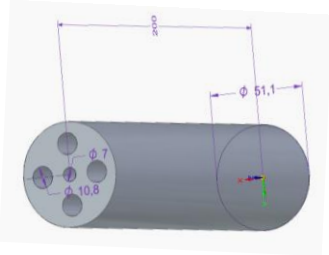
Work in progress

SCALE UP OF STRUCTURED CATALYSTS

Scale-up of the dip/spin coating method (third generation of BCC and GYROID)

Sizes

Type	Size	BCC Cell/Strut (mm)	Gyroid Cell/Strut (mm)
Single-membrane BCC/GYROID (for washcoating)	H=100 mm / Φ_{int} = 15,2 mm , Φ_{ext} = 26,6mm	3/0,4	3/0,6
Single-membrane supports with outer skin (for packed – BCC/GYROID)	H=100 mm / Φ_{int} = 15,2 mm , Φ_{ext} = 26,6mm	3/0,4	3/0,6
Demonstrator: BCC/GYROID for washcoating (4 membranes + 1 thermocouple)	H=100 mm / Φ_{holes} = 15,2 mm, Φ_{ext} = 51,1 mm, Φ_{therm} = 7 mm	3/0,4	3/0,6
Demonstrator with outer skin: for packed – BCC/GYROID (4 membranes + 1 thermocouples)	H=100 mm / Φ_{holes} = 15,2 mm, Φ_{ext} = 51,1 mm, Φ_{therm} = 7 mm	3/0,4	3/0,6



SCALE UP OF STRUCTURED CATALYSTS

Scale-up of the dip/spin coating method (*third generation of BCC and GYROID*)

Amount of catalyst required

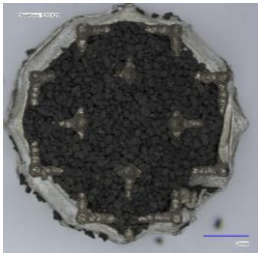
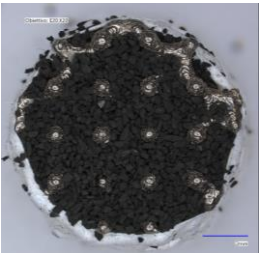
Catalyst Features		COATED POCS Features (Micro-scale)					COATED POCS Features (Prototype) Note: The volume of the holes to host membranes was not removed			
Catalyst code	Formulation	POCS/TPMS Type	POCS/TPMS Volume (cm ³)	Catalyst loaded		Slurry Vol. cm ³	POCS/TPMS Type	POCS/TPMS Volume (cm ³)	Catalyst loaded	
				g	g/cm ³				g	g/cm ³
JM (AN4750)	Ru-based	BCC Cell=3, Strut= 0.4mm , L=1.5cm; Ø=1cm	1,1775	0,261	0,222	16 (for 8-10 POCS) -5g of catalyst	BCC Cell=3, Strut= 0.4mm, L=20 cm; Ø=5,11cm	409,96	90	0,220
JM (AN4750)	Ru-based	GYROID Cell=5, Strut= 0.34mm, L=1.5cm; Ø=1cm	1,1775	0,260	0,221	16 (for 8-10 POCS) - 5g catalyst	GYROID Cell=5, Strut= 0.34mm, L=20cm; Ø=5,11cm	409,96	90	0,220
JM (AN4750)	Ru-based	SINGLE MR - BCC Cell=3, Strut= 0.4mm , L=10cm; Ø=2.66cm with hole (1,08cm)	46,38722	10,200	0,220	155 (For 3-4 POCS), 35g catalyst				

SCALE UP OF STRUCTURED CATALYSTS

Scale-up of packing method (*third generation of BCC and GYROID*)

- Amount of catalyst required

Catalyst Features		PACKED POCS Features (Micro-scale)					PACKED POCS Features (Prototype) Note: The volume of the holes to host membranes was not removed				
Catalyst code	Formulation	POCS Type	POCS Volume (cm ³)	Pellets size	Catalyst loaded		POCS Type	POCS Volume (cm ³)	Pellets size	Catalyst loaded	
					g	g/cm ³				g	g/cm ³
JM (AN4750)	Ru-based	BCC Cell=3, Strut= 0.4mm, L=1.5cm; Ø=1cm	1,177	50-70 mesh – 0,297-0,210mm	1,172	0,995	BCC Cell=3, Strut= 0.4mm, L=20cm; Ø=5,11cm	409,96	50-70 mesh - 0,297-0,210 mm	406	0,990
JM (AN4750)	Ru-based	SINGLE MR – BCC Cell=3, Strut= 0.4mm, L=10cm; Ø=2.66cm with hole (1,08cm)	46,38	50-70 mesh – 0,297-0,210mm	46,10	0,994					



□ Support manufacturing activation and scale-up

- AM can manufacture complex parts allowing more freedom of design optimisation for catalytic reactors compared with traditional manufacturing techniques;
- The combined dip/spin coating method can be used to obtain Structured catalysts with homogeneous and stable catalytic layers (thickness $\approx 17\text{-}41\mu\text{m}$), no pore-clogging phenomena were observed irrespective of the geometry used;
- The presence of anchoring points, and the thermal pre-treatment of supports play a crucial role in achieving high mechanical stability;
- The structured catalytic systems obtained by combining AM with the washcoating technique are characterized by higher porosity (88 -90%), higher SSA ($50\text{-}115\text{ cm}^2/\text{cm}^3$) and lower pressure drops with respect to the conventional packed bed reactor.
- The coating method can be easily scaled up without requiring adjustments compared to samples prepared on a smaller scale

□ Catalytic activity

- The BCC and Gyroid based catalysts have shown promising catalytic performances towards ammonia synthesis and decomposition;
- In particular, the GYROID structure, with its labyrinthine network of channels, provided efficient mass transfer pathways;
- The Gyroid structure enabled the design of lighter and more compact reactors, addressing weight and volume constraints in applications like distributed hydrogen production and ammonia synthesis.
- Overall, this comparative analysis highlights the importance of structural design in catalytic processes and underscores the potential of GYROID structures for advancing reactor efficiency and compactness.

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Thanks!



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